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FIG. 1

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FIG. 2

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FIG. 3A

STRAIGHT BLADE

FIG. 3B

SPIRAL BLADE

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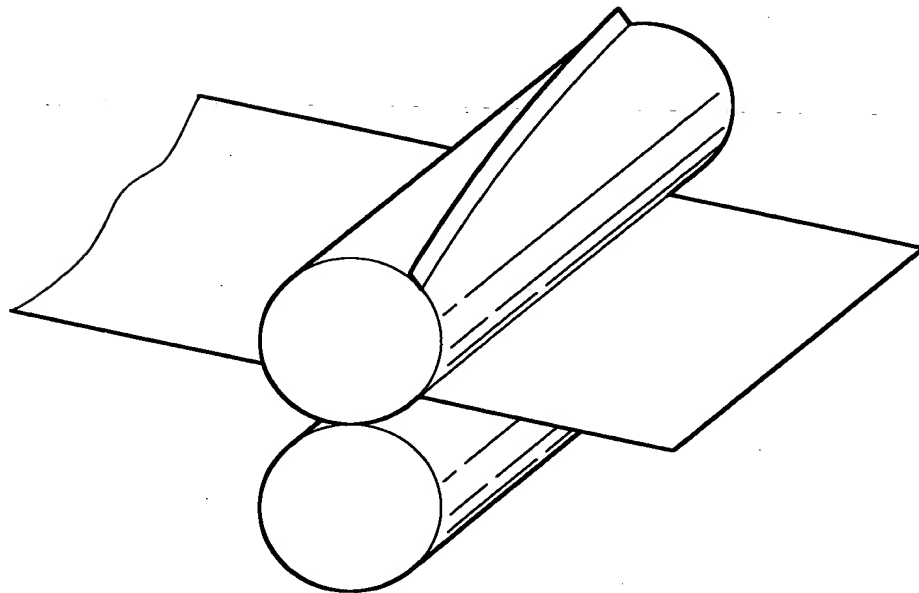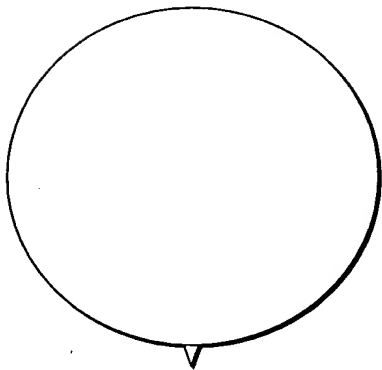## FIG. 4A

SINGLE BLADE

FIG. 4B

DOUBLE BLADE
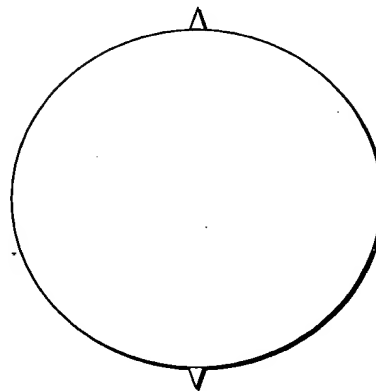
FIG. 4C

TRIPLE BLADE

FIG. 4D

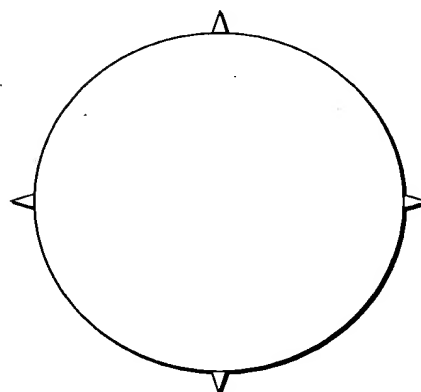QUADRUPLE BLADE
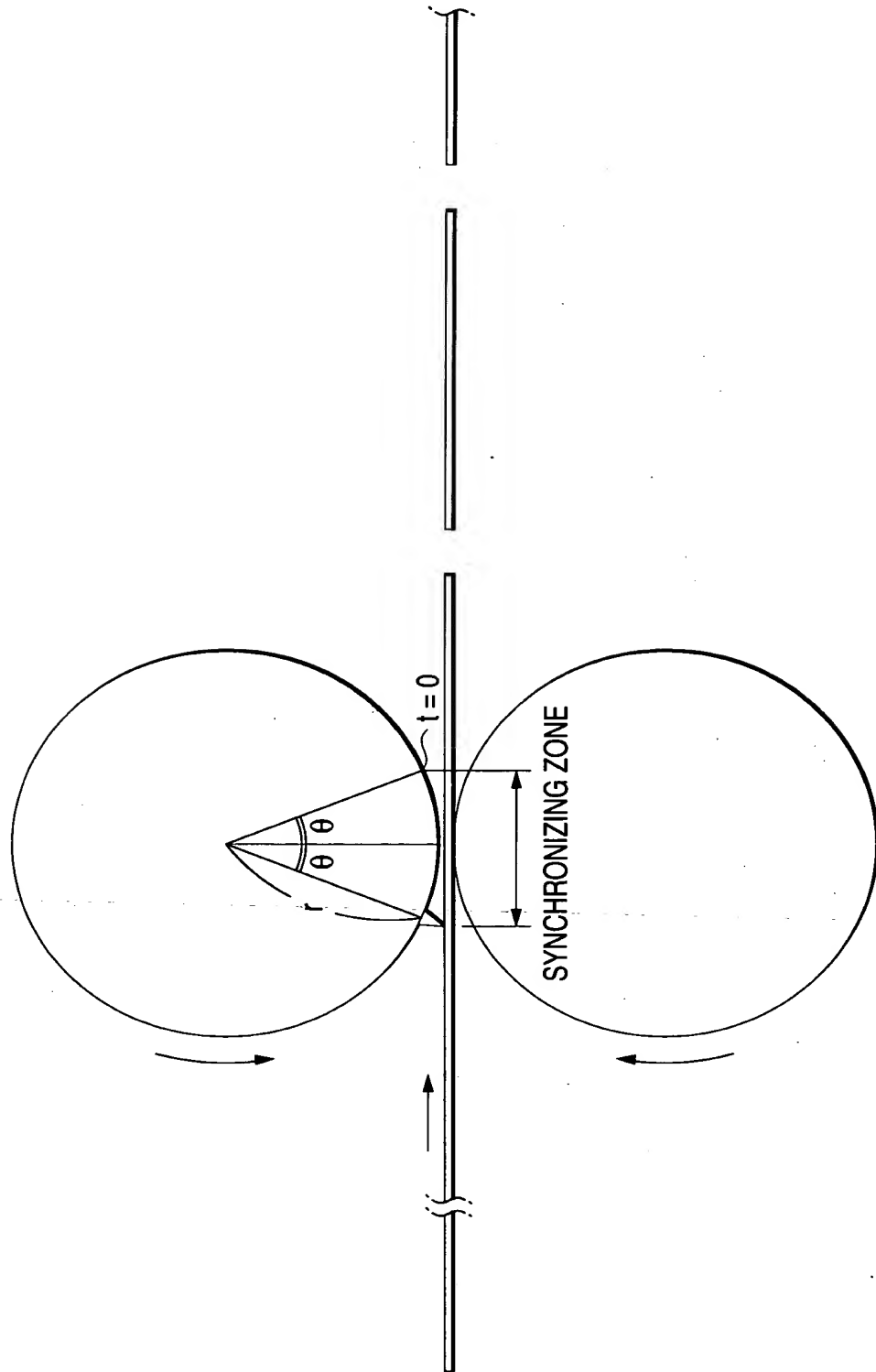
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FIG. 5

t = 0

θ

θ

r

SYNCHRONIZING ZONE
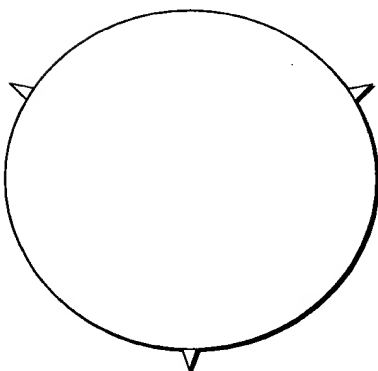
[CASE OF SPIRAL BLADE]

FIG. 6A

FIG. 6B

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FIG. 7A

x (rev)

POSITION

X₂ ─────────────────────── B (T₂, X₂)

X₁ ──── A (T₁, X₁)

0   T₁   T₂   t (SEC)

FIG. 7B

v (rps)

SPEED

V₂ ────────────────────── (T₂, V₂)
V₁ ──── (T₁, V₁)

0   T₁   T₂   t (SEC)

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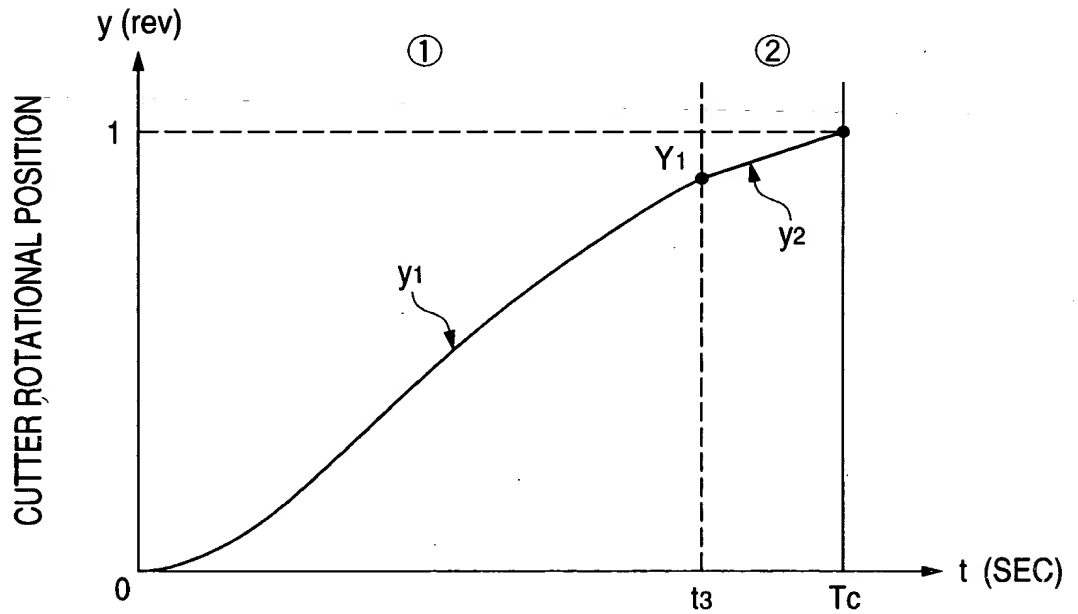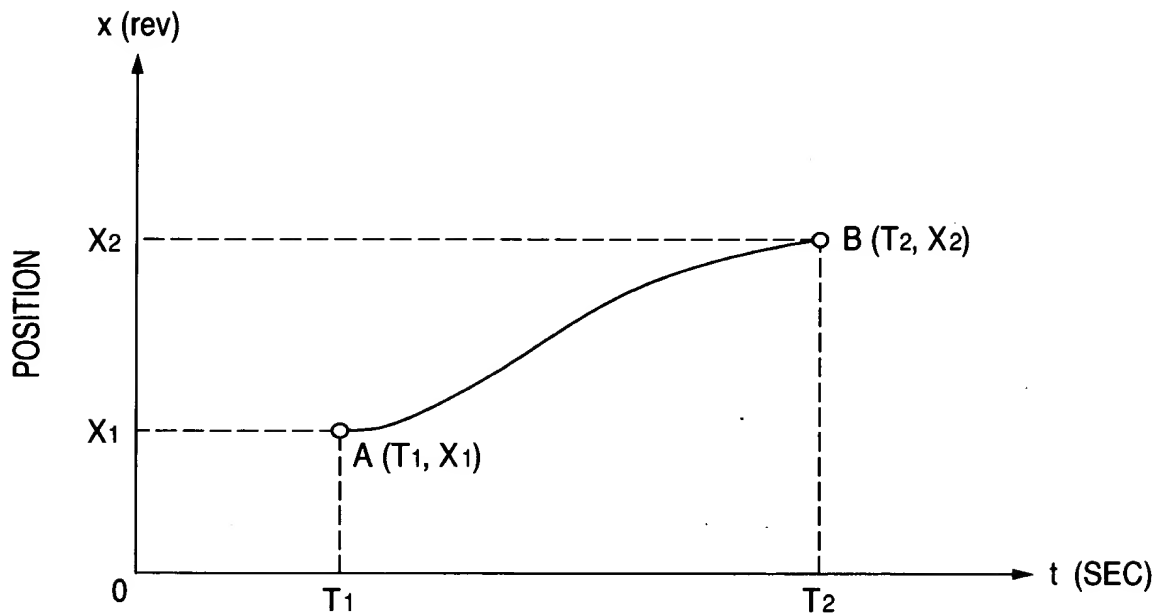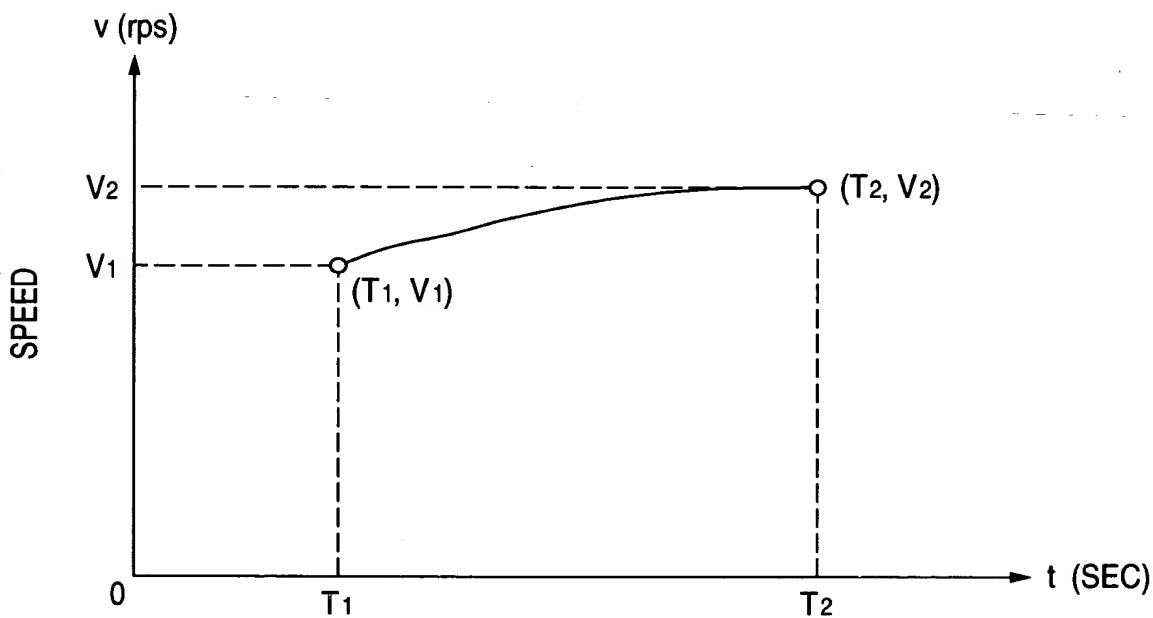3 of 24
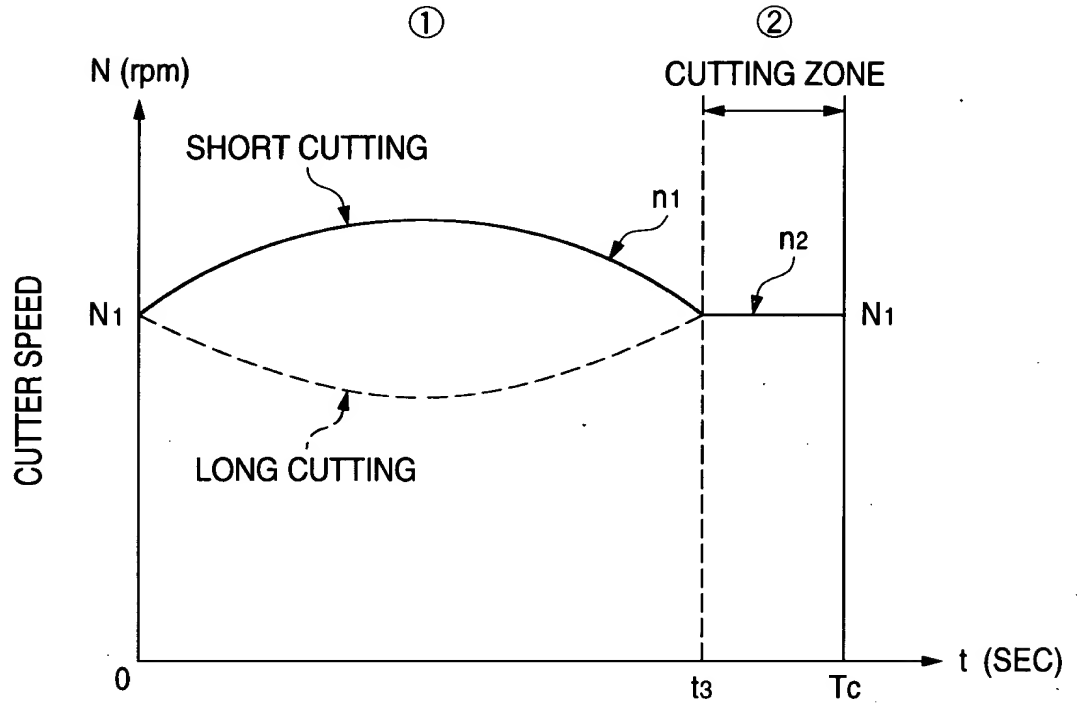
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FIG. 8

(CAM CURVE EQUATIONS OF SPIRAL BLADE)

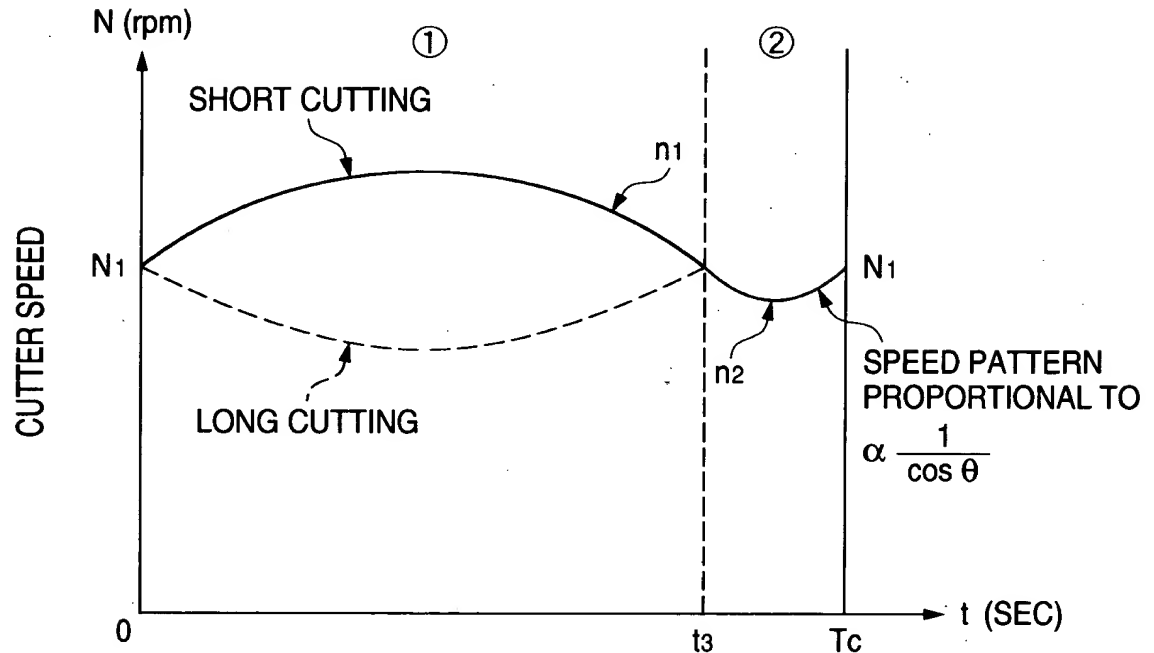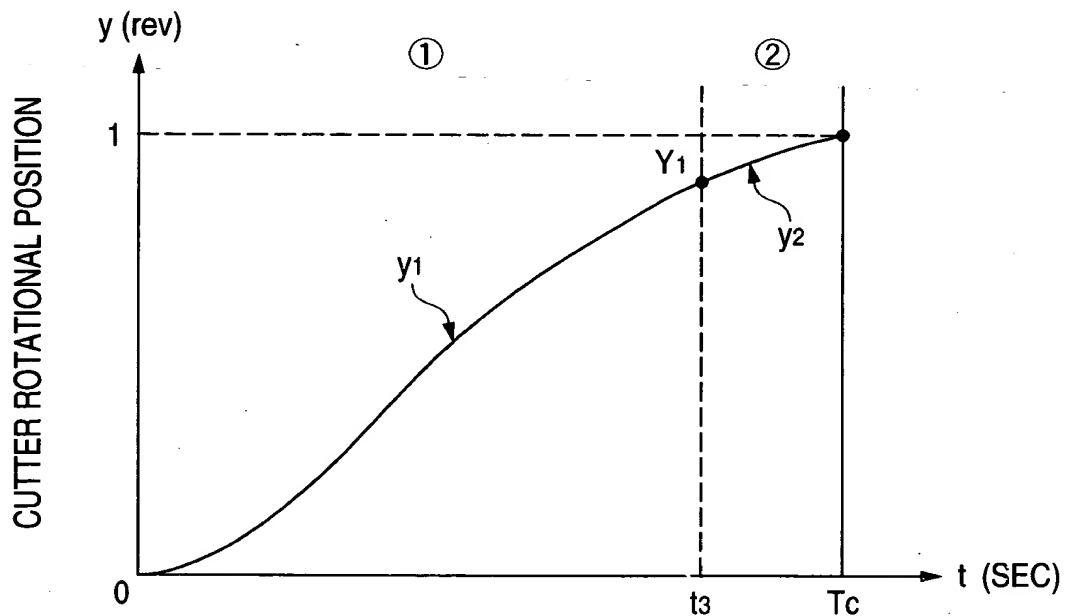| ZONE	CUTTER ROTATIONAL SPEED n (rpm)	CUTTER ROTATIONAL POSITION y (rev)
①	$n_1 = 60\,(3At^2 + 2Bt + C)$	$y_1 = At^3 + Bt^2 + Ct + D$
②	$n_2 = N_1$	$y_2 = \dfrac{(1 - Y_1)}{(T_C - t_3)}\,(t - T_C) + 1$

[CASE OF STRAIGHT BLADE]

FIG. 9A

N (rpm)   ①   ②

SHORT CUTTING
                                    n1

CUTTER SPEED

N1   N1
                                    n2
                              SPEED PATTERN
                              PROPORTIONAL TO
LONG CUTTING
                              $\alpha \dfrac{1}{\cos\theta}$

0   t3   Tc   t (SEC)

FIG. 9B

y (rev)   ①   ②

1   Y1
                                    y2

CUTTER ROTATIONAL POSITION

                    y1

0   t3   Tc   t (SEC)

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FIG. 10

(CAM CURVE EQUATIONS OF STRAIGHT BLADE)

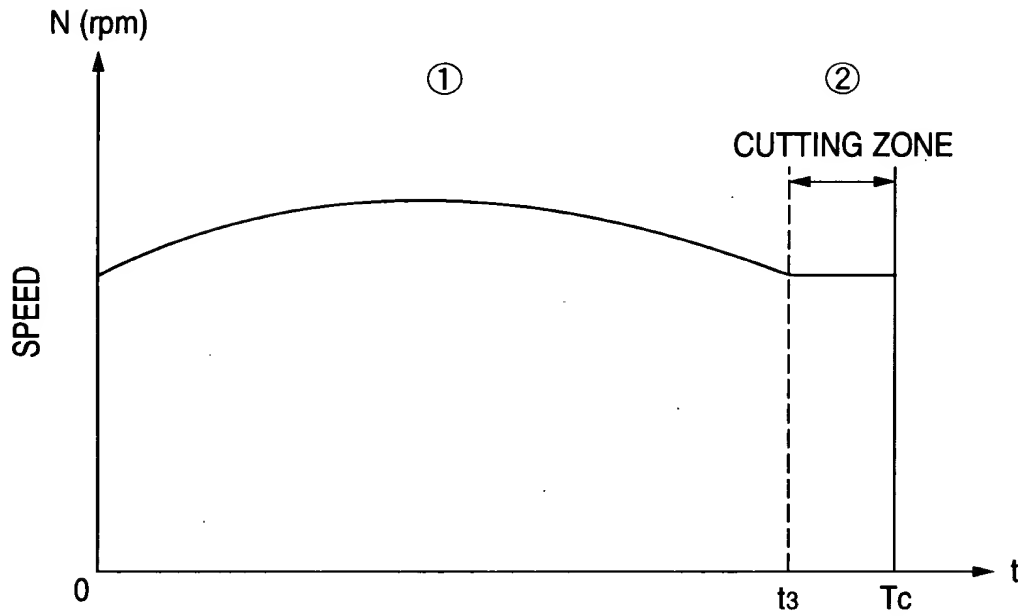| ZONE	CUTTER ROTATIONAL SPEED n (rpm)	CUTTER ROTATIONAL POSITION y (rev)
①	$n_1 = 60\,(3At^2 + 2Bt + C)$	$y_1 = At^3 + Bt^2 + Ct + D$
②	$n_2 = \dfrac{60}{2\pi\sqrt{\left(\dfrac{r}{V_0}\right)^2 - \left(t - \dfrac{t_3 + T_C}{2}\right)^2}}$	$y_2 = \dfrac{1}{360}\sin^{-1}\left\{\left(\dfrac{V_0}{r}\right)(t - \dfrac{t_3 + T_C}{2})\right\} + G$ $\left(G = 1 - \dfrac{\theta_0}{360}\right)$ (UNIT OF $\sin^{-1}x$: (°))

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FIG. 11A

FIG. 11B

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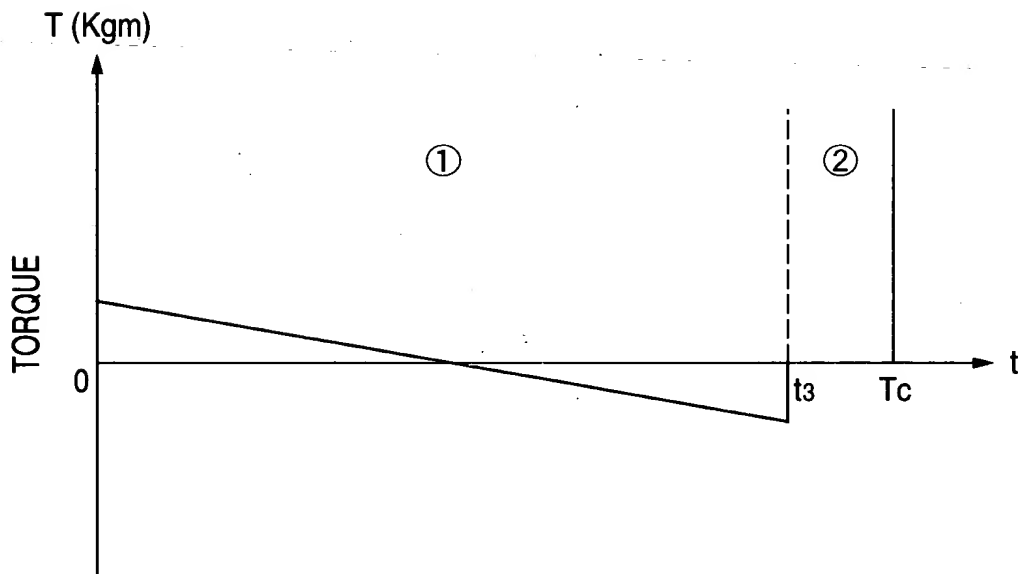Darryl Mexic   202-293-7060
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FIG. 12A

[SPEED PATTERN OF QUADRATIC FUNCTION WAVEFORM]

N (ABSOLUTE NUMBER)
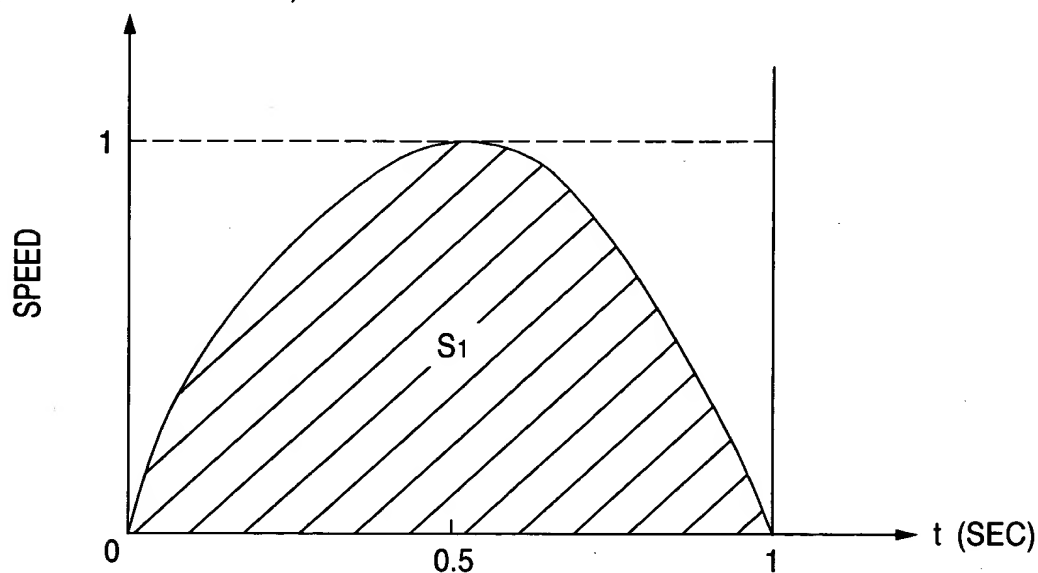
FIG. 12B

[SPEED PATTERN OF TRAPEZOIDDAL WAVEFORM]

N (ABSOLUTE NUMBER)

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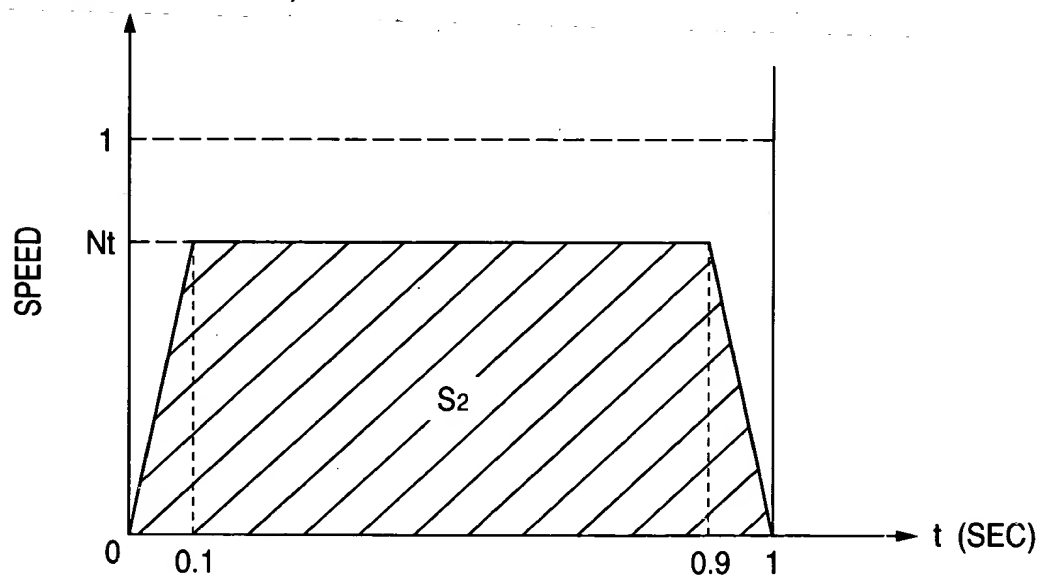13 of 24

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FIG. 13A

[SPEED PATTERN OF GENERALIZED TRAPEZOIDAL WAVEFORM]

N (ABSOLUTE NUMBER)

FIG. 13B

αrms ≥ 2.45

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FIG. 14

LV CURVE

LINE SPEED

v (m/MIN)

CONVENTIONAL SYSTEM

PRESENT SYSTEM

0

CUTTING LENGTH (mm)

SHORT ← PERIPHERAL LENGTH → LONG

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FIG. 15

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METHOD OF CONTROLLING AN ELECTR●
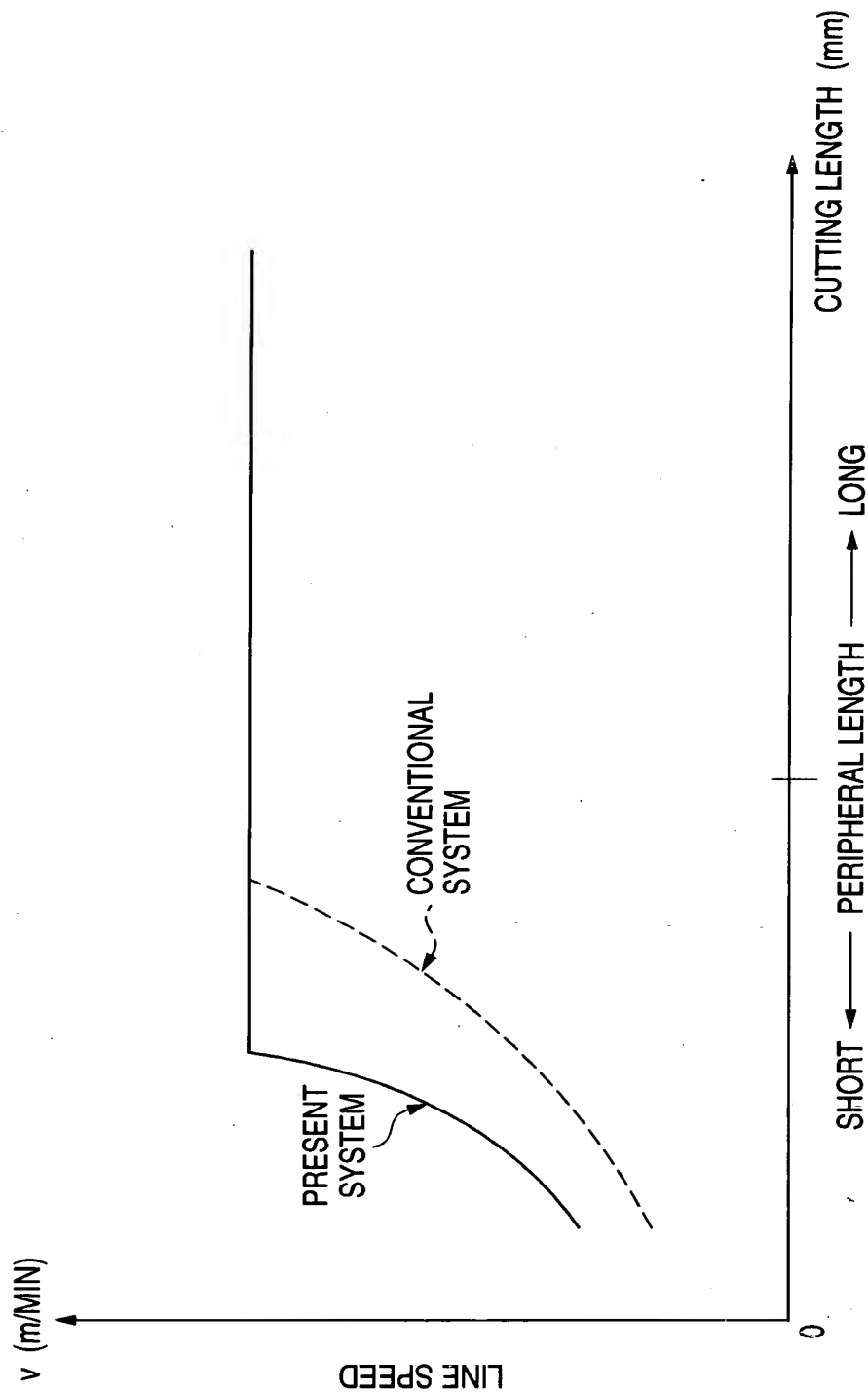CAM TYPE ROTARY CUTTER, AND METH
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FIG. 16A   [SINGLE HEATER LATERAL SEALING MECHANISM]

← FILM

HEATER SURFACE

HEATER SURFACE

LATERAL SEALING MECHANISM

LATERAL SEALING MECHANISM
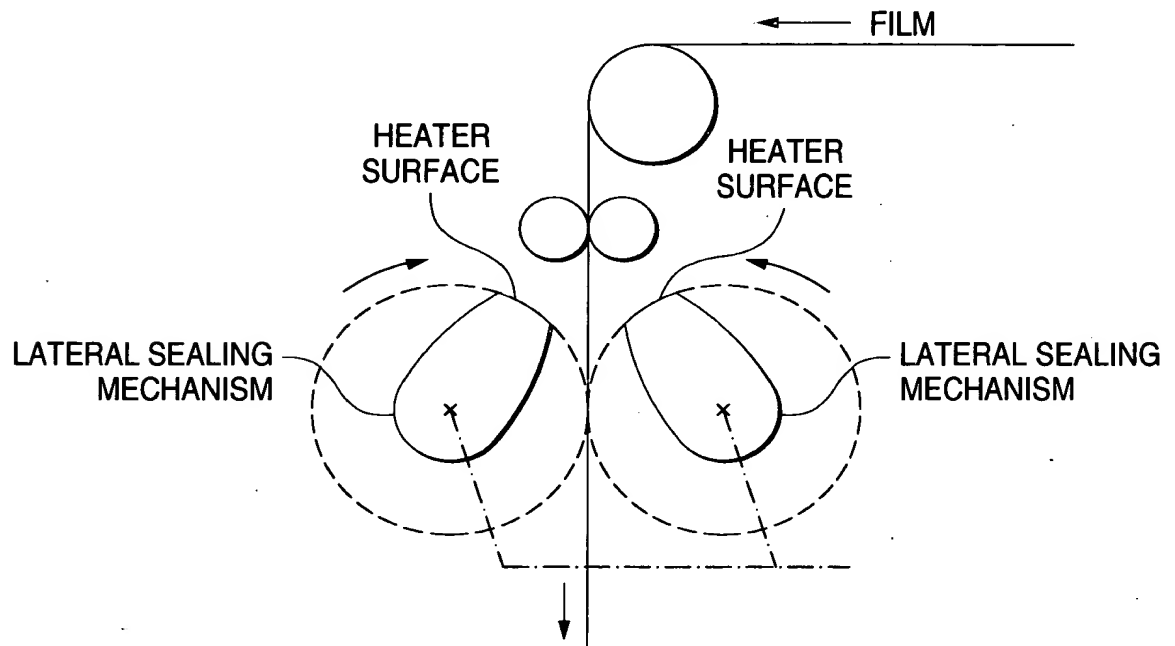
FIG. 16B   [DOUBLE HEATER LATERAL SEALING MECHANISM]

← FILM

HEATER SURFACE

HEATER SURFACE

46a

46b

HEATER SURFACE

HEATER SURFACE

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FIG. 17

DOUBLE HEATER (M = 2)

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FIG. 18A

①   ②

SEALING ZONE

N (rpm)

ROTATIONAL SPEED OF LATERAL SEALING MECHANISM

$$\text{BAG LENGTH} < \left(\frac{\text{PERIPHERAL LENGTH}}{M} \right)$$

n_1

n_2

N_1

$$\text{BAG LENGTH} > \left(\frac{\text{PERIPHERAL LENGTH}}{M} \right)$$

$$\text{BAG LENGTH} = \left(\frac{\text{PERIPHERAL LENGTH}}{M} \right)$$

0   t_3 T_c t

t_0

FIG. 18B

y (rev)

ROTATIONAL POSITION OF LATERAL SEALING MECHANISM

①   ②

$\frac{1}{M}$

Y_1

y_2

y_1

0   t_3 T_c t

t_0

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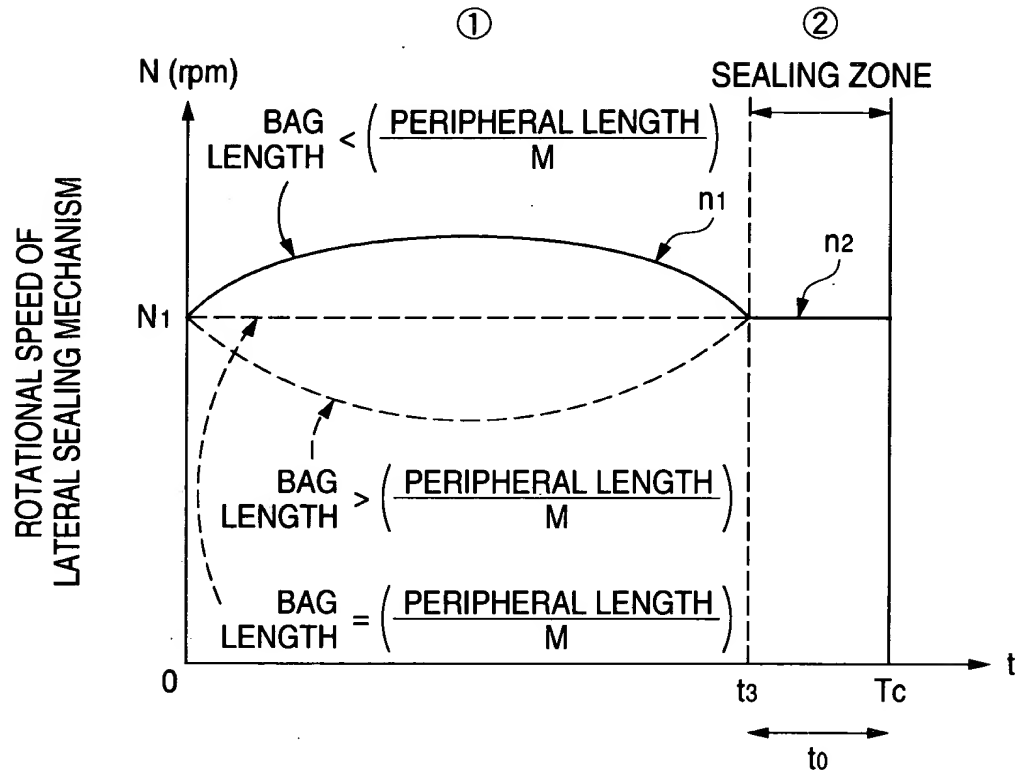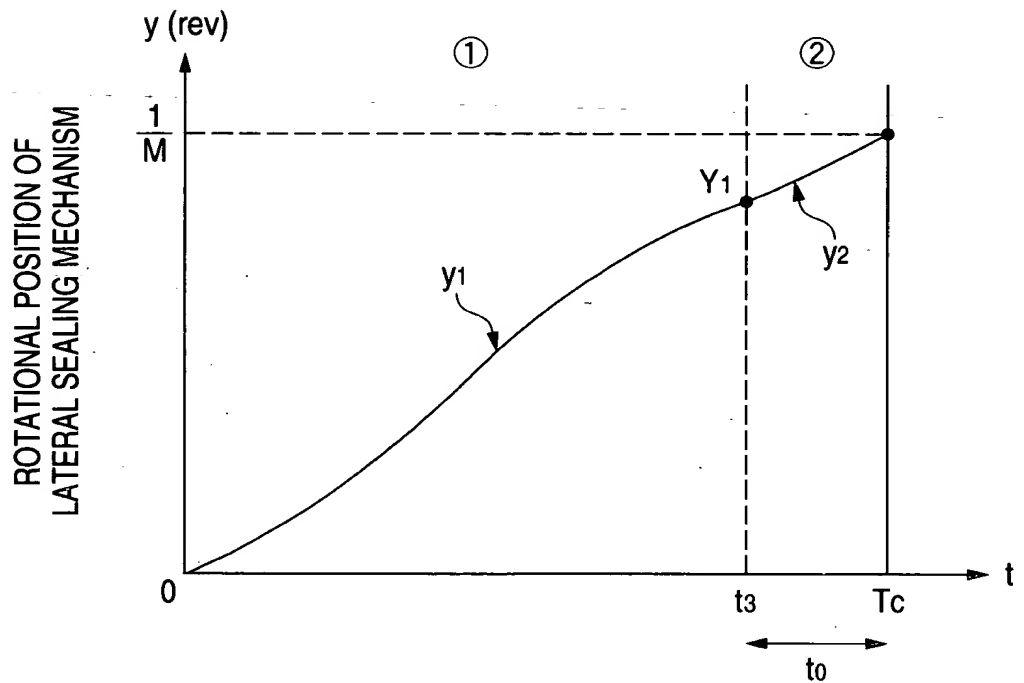Filed: July 11, 2001
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FIG. 19

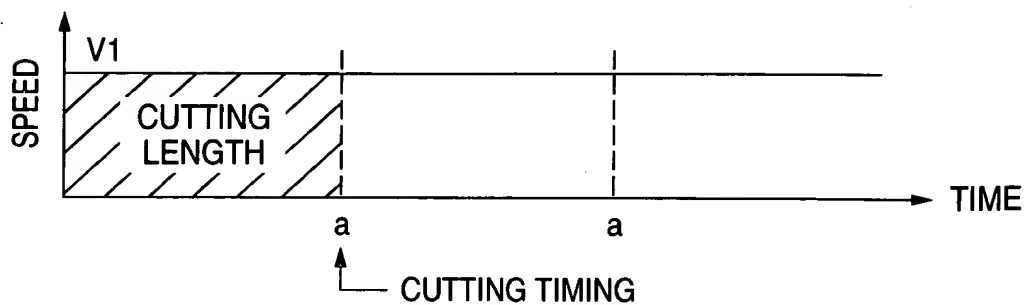| ZONE	ROTATIONAL SPEED OF LATERAL SEALING MECHANISM n (rpm)	ROTATIONAL POSITION OF LATERAL SEALING MECHANISM y (rev)
① NON SEALING ZONE	$n_1 = 60 \ (3At^2 + 2Bt + C)$	$y_1 = At^3 + Bt^2 + Ct + D$
② SEALING ZONE	$n_2 = N_1 \cdot$ (CONSTANT)	$y_2 = \dfrac{\frac{1}{M} - Y_1}{Tc - t_3}(t - Tc) + \dfrac{1}{M}$

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FIG. 20

WORK PIECE →

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FIG. 21A

SPEED

V1

CUTTING
LENGTH

TIME

a   a

CUTTING TIMING

FIG. 21B

SPEED

V2

PERIPHERAL
LENGTH

TIME

b

FIG. 21C

SPEED

CUTTING COMPLETION SIGNAL

V2

START

TIME

FIG. 21D

CUTTING TIMING

SPEED

V3

PERIPHERAL
LENGTH

TIME

a   b

FIG. 21E

SPEED

⊖ COMMAND

TIME

FIG. 21F

SPEED

TIME

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FIG. 22

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FIG. 23

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FIG. 24A

FIG. 24B